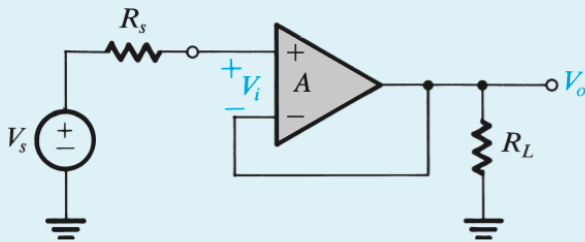


## EE304 – Problem Set 5

### Problem 11.3 [S&S 7/e]

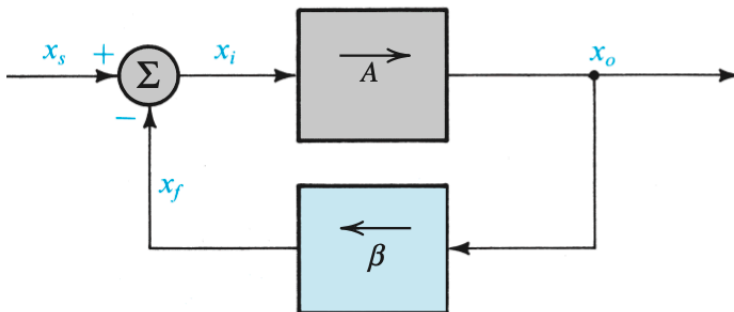
**11.3** The noninverting buffer op-amp configuration shown in Fig. P11.3 provides a direct implementation of the feedback loop of Fig. 11.1. Assuming that the op amp has infinite input resistance and zero output resistance, what is  $\beta$ ? If  $A = 1000$ , what is the closed-loop voltage gain? What is the amount of feedback (in dB)? For  $V_s = 1$  V, find  $V_o$  and  $V_i$ . If  $A$  decreases by 10%, what is the corresponding percentage decrease in  $A_f$ ?



**Figure P11.3**

### Problem 11.10 [S&S 7/e]

**11.10** For the negative-feedback loop of Fig. 11.1, find the loop gain  $A\beta$  for which the sensitivity of closed-loop gain to open-loop gain [i.e.,  $(dA_f/A_f)/(dA/A)$ ] is  $-40$  dB. For what value of  $A\beta$  does the sensitivity become  $1/5$ ?

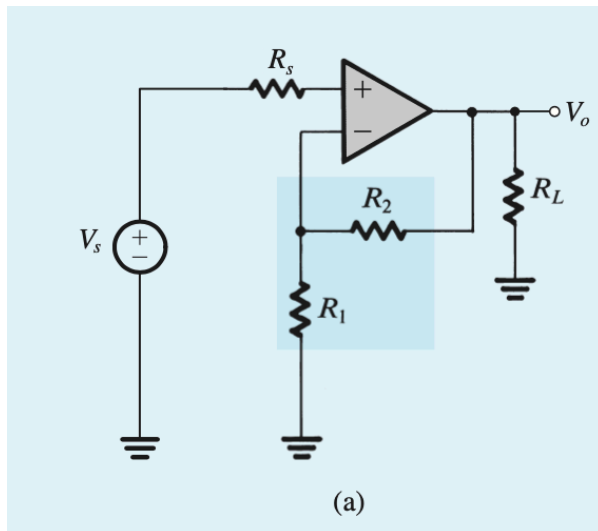


**Figure 11.1** General structure of the feedback amplifier. This is a signal-flow diagram, and the quantities  $x$  represent either voltage or current signals.

*Problem 11.27 [S&S 7/e]*

**D 11.27** Consider the series–shunt feedback amplifier in Fig. 11.11(a), which is analyzed in Example 11.3.

- If  $R_1 = 10 \text{ k}\Omega$ , find the value of  $R_2$  that results in an ideal closed-loop gain of 10.
- Use the expression for  $A\beta$  derived in Example 11.3 to find the value of the loop gain for the case  $\mu = 1000$ ,  $R_{id} = 100 \text{ k}\Omega$ ,  $r_o = 1 \text{ k}\Omega$ ,  $R_s = 100 \text{ k}\Omega$ , and  $R_L = 10 \text{ k}\Omega$ . Hence determine the value of the closed-loop gain  $A_f$ .
- By what factor must  $\mu$  be increased to ensure that  $A_f$  is within 1% of the ideal value of 10?



**Figure 11.11** Example 11.3. (a) A series–shunt feedback amplifier;

*Expression of  $A\beta$  derived in Example 11.3:*

$A\beta \equiv -V_r/V_t$  involves repeated application of the voltage divider rule, resulting in

$$A\beta = \mu \frac{\{R_L \parallel [R_2 + R_1 \parallel (R_{id} + R_s)]\}}{\{R_L \parallel [R_2 + R_1 \parallel (R_{id} + R_s)]\} + r_o} \times \frac{[R_1 \parallel (R_{id} + R_s)]}{[R_1 \parallel (R_{id} + R_s)] + R_2} \times \frac{R_{id}}{R_{id} + R_s}$$

Problem 11.83 [S&S 7/e]

**11.83** An op amp designed to have a low-frequency gain of  $10^5$  and a high-frequency response dominated by a single pole at 100 rad/s acquires, through a manufacturing error, a pair of additional poles at 20,000 rad/s. At what frequency does the total phase shift reach  $180^\circ$ ? At this frequency, for what value of  $\beta$ , assumed to be frequency independent, does the loop gain reach a value of unity? What is the corresponding value of closed-loop gain at low frequencies?

Problem 11.86 [S&S 7/e]

**11.86** Consider a feedback amplifier for which the open-loop gain  $A(s)$  is given by

$$A(s) = \frac{10,000}{(1 + s/10^4)(1 + s/10^5)^2}$$

If the feedback factor  $\beta$  is independent of frequency, find the frequency at which the phase shift is  $180^\circ$ , and find the critical value of  $\beta$  at which oscillation will commence.